

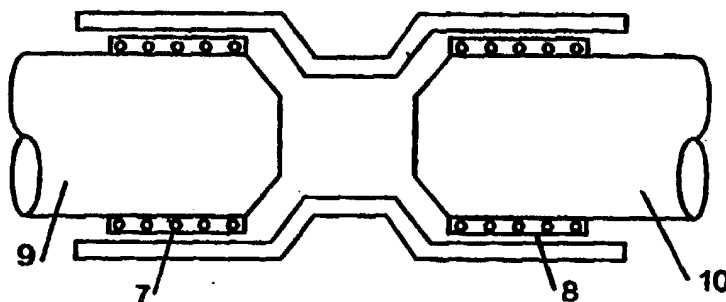
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**(54) Title:** HEAT FUSION FITTING**(57) Abstract**

A method for the manufacture of a heat fusion fitting, which comprises i) forming a body (1) comprising at least a first layer of a first cross-linked polymeric material, ii) embedding or partly embedding a ferromagnetic heating element (11, 12) in a second polymeric material (13, 14) to form an insert (7, 8), the ferromagnetic heating element (11, 12) having a Curie temperature equal to or greater than the crystalline melting point or softening point of the second polymeric material (13, 14), and iii) assembling the body and the insert (7, 8) to form the fitting.



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### HEAT FUSION FITTING

This invention relates to heat fusion fittings, and more particularly to an improved method for the manufacture of  
5 heat fusion fittings and to new heat fusion fittings and pipe joints produced thereby.

heat fusion fittings comprising in-line couplings, T-joints, bends, saddle fittings, patches and similar  
10 devices have been known for many years. In a typical heat fusion fitting, an electrical resistance heater element is embedded in the inner surface of a sleeve of a thermoplastic polymeric material, the sleeve being adapted to fit over a plastic pipe or pipes to be  
15 connected. Such fittings are conventionally termed electrofusion fittings.

In an in-line coupling the pipes are inserted into the sleeve into abutment with one another, or into abutment  
20 with a stop member, and the heater elements are then energised. Upon heating of the heater elements, the adjacent regions of the sleeve are softened to the point of fusion, whereby the polymeric materials of the pipes and sleeve are fused together.

25

Essentially the same approach is employed for saddles and patches except that conventional means are employed to hold the elements in intimate contact prior to completion of the fusion process.

US Patent No 2739829 takes a slightly different approach using induction heating as opposed to resistance heating. Strips of metallic material are placed between a sleeve and pipes to be joined at two locations spaced from the abutment region of the two pipes. A coil connected to an AC source is employed to heat the metallic strips to produce fusion of the polymeric material of the sleeve with the polymeric material of the pipes. Other patents disclosing the use of induction heating in heat fusion fittings include, for example, W080/02124, EP-A 0572546, EP-A-0513391, and US 4256945. The entire disclosures of each and every one of the abovementioned patents are incorporated herein by reference for all purposes.

Heat fusion fittings are conventionally manufactured by injection moulding the entire plastics body of the fitting over the metallic heating element. This is because of the need to locate the heating element or elements accurately within the fitting in order to leave so-called "cold zones" or unheated areas at the ends of the fitting, and adjacent the abutment region of the pipes, in the case of an in-line coupling, to prevent escape of fused polymeric material from the melt fusion regions.

Various efforts have been made to find a more cost effective method for the manufacture of heat fusion fittings, for example, by extruding a tubular polymeric

sleeve, heating the sleeve, inserting the electrical resistance heating element into the sleeve on a mandrel which simultaneously expands the sleeve, removing the mandrel and allowing the sleeve to contract around the heating element. Various methods of this type are described in Swiss Patent No 544906, DE-A-2302458, GB-A-2036518 and in US 4362684, the entire disclosures of which are incorporated herein by reference for all purposes. In US 4362684 it is stated that the simultaneous widening and sliding of the tubular sleeve body onto the heating coil create radial contraction strains in the tubular body which produce welding pressure and facilitate bonding of the pipes. However, in practice, it is found that any such effects are minimal, since the radial contraction strains in the sleeve are dissipated after a very short time, and the fusion process produces only a relatively localised heating such that the main body of the sleeve remains relatively cold and could not possibly contract to produce a welding pressure as suggested in US 4362684. Further difficulties also arise in connectorising electrical resistance heating elements inserted into a tubular sleeve body in this way.

For whatever reason, to the best of the Applicants' knowledge, none of the abovementioned methods have been put into practice commercially, and the method of choice

for the manufacture of heat fusion fittings remains injection moulding.

In US5189271 there is disclosed a connector comprising a  
5 heat shrinkable sleeve heated by a ferromagnetic member which in turn is heated by a varying magnetic field, the ferromagnetic member having a Curie temperature above the shrink temperature of the sleeve.

10 In a further and separate development, for plastics pipes having improved temperature and pressure resistance, it has been proposed, for example, in US 4927184, to use a pipe wall comprising at least a layer of a cross-linked polyolefin material. Pipelines including such pipes also  
15 require higher strength fittings, and US 4927184 also suggests that the fitting can comprise an outer layer of a cross-linked polyolefin material. It is suggested that if the cross-linked outer layer of the fitting is heated, it will be subject to a contraction, exerting a pressure  
20 on the pipes, but this would appear very unlikely, as the cross-linked outer layer is not expanded, and in the heat fusion process it would remain relatively cold. It is also suggested that the fitting can be extruded, but no information is given as to how this production method  
25 could be put into practice. The entire disclosure of US 4927184 is incorporated herein by reference for all purposes.

According to the present invention, there is provided a heat fusion fitting comprising a body comprising at least an outer layer of cross-linked polymeric material and an induction heating element in contact with the body.

5

In a first aspect, the invention provides a method for the manufacture of a heat fusion fitting, which comprises:

- 10 (i) forming a body comprising at least a first layer of a first cross-linked polymeric material,
- (ii) embedding or partly embedding a ferromagnetic heating element in a second polymeric material to form an insert, the ferromagnetic heating element having a Curie temperature equal to or greater than the crystalline melting point or softening point of the
- 15 second polymeric material, and
- 20 (iii) assembling the body and the insert to form the fitting.

- 25 In another aspect, the invention provides a heat fusion fitting comprising a body comprising at least a first layer of a first cross-linked polymeric material, a second layer of a second polymeric material, and a

ferromagnetic heating element, the ferromagnetic heating element being embedded or partly embedded in the second layer and having a Curie temperature equal to or greater than the crystalline melting point or softening point of  
5 the second polymeric material.

In a further aspect, the invention provides a kit of parts for a heat fusion fitting, the kit of parts comprising a body and an insert, the insert comprising a  
10 ferromagnetic heating element embedded or partly embedded in a fusible polymeric material, the ferromagnetic heating element having a Curie temperature equal to or greater than the crystalline melting point or softening point of the polymeric material, and the body being  
15 adapted to receive the insert and comprising at least a first layer of a first cross-linked polymeric material.

In the majority of applications, the fitting will, in use, be positioned over a pipe end or spigot to be  
20 connected and the invention will henceforth be more particularly described with respect to such an external fitting. In such cases, the first layer of a first cross-linked polymeric material will be an outer layer of the body and the second layer of a second polymeric  
25 material will be an inner layer, with the insert being positioned internally of the body. It will be appreciated, however, that the fitting could also be an internal coupler, whereupon the first layer would become



the inner layer of the body and the second layer would become the outer layer of the body, the insert then being positioned externally of the body, and that such fittings are also included within the invention.

5

The body of the fitting will generally be of hollow, tubular construction, although other shapes are possible depending upon the application. The body can be wholly or partly formed of cross-linked polymeric material, but at least an outer layer will be so formed. The body can, for example, be of a dual layer or multiple layer construction, with one or more outer cross-linked layers surrounding one or more uncross-linked layers. A body of dual layer or multiple layer construction can be of particular value in fittings used for connecting pipes of dual or multiple layer construction. Such pipes can comprise, for example, various barrier layers and tie layers. Examples of barrier layers include benzene barrier layers such as nylon and PBT layers, oxygen barrier layers such as EVOH, and water barrier layers such as PVCC. The body of the fitting can also comprise such barrier layers and tie layers as appropriate.

25 Preferably the body is shaped such that it can be produced by continuous extrusion methods, for example, as disclosed in PCT/EP96/02801, the entire disclosure of which is incorporated herein by reference for all

purposes. The body can, as previously stated, be of a tubular construction and may also be extruded with corrugations or ribs on its outer surface. A body with a corrugated outer surface or portion thereof can provide  
5 a fitting which is bendable such that a pipe bend can be formed at the fitting. On the other hand, a body with a ribbed outer surface can provide a fitting having improved ring stiffness. An advantage of the present invention is that the body does not need to be produced  
10 with moulded-in terminals, which has complicated and increased the cost of prior art processes. Such projecting terminals are also a serious disadvantage if the pipe and fitting are to be used in no-dig applications where the pipe is pulled through the ground,  
15 because the projecting terminals add considerable drag resistance.

The first polymeric material is preferably a polyolefin or an olefin copolymer. Suitable polymeric materials  
20 include, for example, polymers, copolymers and polymeric blends of ethylene, propylene, butylene, pentene, styrene, butadiene, vinyl alcohols, esters and amides, vinyl halides and similar monomers. Polyethylene, ethylene copolymers, PVC and modified PVC are the  
25 preferred first polymeric materials for use in the present invention.

The first polymeric material can be cross-linked, for example, by the use of chemical cross-linking agents, for example, peroxides, silanes and similar materials, or by the use of irradiation, for example, electron beam  
5 irradiation, or UV light irradiation, using suitable cross-linking promoters, such as triallyl cyanurate. Chemical cross-linking during extrusion is the preferred route, for example, as disclosed in PCT/EP96/02801.

10 The first polymeric material is preferably cross-linked to an extent of at least 30%, preferably to an extent of from 30% to 95%. The degree of cross-linking in this specification is expressed as gel content, and measured using the method of ASTM. Cross linking the first layer  
15 can, of course, improve the ring strength of the fitting, which may be advantageous for fittings used in the jointing of cross-linked pipes.

In a particularly preferred method according to the  
20 invention, the body and the insert are assembled by imparting a degree of dimensional recoverability to the body, such that the body, or a portion thereof, can recover from a larger diameter to a smaller diameter and thereby engage the insert which is positioned in the  
25 direction of recovery. In general, the body will recover from a deformed, usually expanded, configuration, although this is by no means essential, and the body can be recoverable due to stresses induced, for example,

during extrusion. Where the body recovers from the expanded configuration, the recovery can be elastic recovery, due to elastomeric forces, or heat recovery. In heat recoverability, the body is expanded by a  
5 temperature above the crystalline melting point or softening point of the first cross-linked polymeric material and cooled whilst in its expanded configuration. The body then retains its expanded configuration until again heated above the crystalline melting point or  
10 softening point of the first polymeric material, whereupon the body will attempt to recover to its original configuration.

Preferably, however, the body is expanded at a  
15 temperature below the crystalline melting point or softening point of the first polymeric material, for example, as described in WO93/05332 and WO94/18486, the entire disclosures of which are incorporated herein by reference for all purposes.

20

The body of the heat fusion fitting can be expanded, for example, using a mandrel, by differential gas pressure, or any other suitable means. Expansion preferably takes place below the crystalline melting point or softening  
25 point of the first cross-linked polymeric material and can produce considerable strains in the three-dimensional cross-linked polymeric lattice. Because of the presence of the cross-links, these strains cannot readily be

dissipated in the material by relaxation, and thus, after removal of the expansion forces, the body will tend to recover towards its original configuration. The recovery time differs for different polymeric materials, but in  
5 the case of cross-linked polyethylene, can take up to several minutes, for example, from about 5 - 30 seconds, depending upon the diameter/wall thickness ratio.

Care must be taken in expanding the body not to introduce  
10 cracks or splits in the body. In general, the expansion of the body is usually in the range of from 15% to 45%. In the case of cross-linked polyolefins, the required expansion can usually be achieved at room temperature, but for certain other polymeric materials gentle heating  
15 may be necessary. It is, however, a significant advantage of the present invention that the expansion can be carried out at low temperatures, due to the presence of the cross-links in the first polymeric material.

20 Not all of the body of the fitting may need to be expanded to allow for insertion of the heating elements. For example, in producing an in-line coupling, it may only be necessary to expand the end sections, because the mid-section, where the pipe ends abut, is preferably a  
25 cold spot, without any heating.

Certain polymers, such as PVC, can be made to be recoverable without cross-linking, and these can also be

used and expanded to produce the body of the fitting in appropriate cases.

One or more inserts can be used in the fitting and method  
5 of the invention. The insert or inserts are formed by  
embedding or partly embedding a ferromagnetic heating  
element in a second polymeric material. Suitable  
ferromagnetic heating elements are disclosed in the  
patent specifications mentioned hitherto, but preferably  
10 the heating element comprises a wire of copper or like  
conductive material covered with a ferromagnetic material  
as described in US4256945. The wire can be, for example,  
formed into a spiral with cross members, a plurality of  
widely spaced rings also with cross members, a mesh of  
15 widely spaced wires forming large squares, or the like.  
Due to the fact that the ferromagnetic material surrounds  
the wires in the preferred configuration, demagnetising  
(edge) effects are not present. Furthermore, the  
arrangement of a ferromagnetic material on a copper wire  
20 behaves as set forth in US 4256945, and temperature  
regulation is excellent and occurs incrementally along  
the wires so that the temperature is substantially  
uniform throughout. Preferred ferromagnetic heating  
elements are described and claimed in WO92/15182. The  
25 entire disclosure of WO92/15182 is incorporated herein by  
reference for all purposes.

Preferably, the ferromagnetic heating element is of a generally tubular construction and is preferably inwardly radially deformable, at least when the second polymeric material has become fused. The ferromagnetic heating element can, for example, be in the form of a radially inwardly deformable wire cage, or a cage of usually corrugated or perforated metal wherein the corrugations or perforations assist inward deformation. Alternatively, the element may be in the form of a so-called "chinese finger" which can elongate with a reduction in diameter. In another possibility, the ferromagnetic heating element can comprise ferromagnetic particles that are dispersed in a polymeric material, for example, as described in US5189271. The fusion of the polymeric material, in this embodiment, permits radial deformation of the ferromagnetic heating element. Inward radial deformation of the ferromagnetic heating element, for example, by recovery of the body of the fitting, can assist in improving the fusion bond by improving mixing in the fusion zone. In addition, if the element is provided with projections, for example, sharp teeth, which can cut into the surface of the pipe to be connected, bonding and pull-out strength can be further improved.

25

The (second) (polymeric) (material) can comprise any of the polymeric materials listed earlier in connection with the first polymeric material and can be the same or different

from the first polymeric material. The second polymeric material can, if desired, have adhesive properties, at least in the molten state, and, for example, polymeric materials comprising hot melt adhesives, for example, 5 polyamides and ethylene/vinyl acetate polymers can also be used. The second polymeric material is preferably uncross-linked, however, or at least is cross-linked to only a small extent, preferably less than 35%, more preferably less than 5%, so that it is still capable of 10 melt fusion. The second polymeric material is preferably uncross-linked polyethylene. The insert is preferably formed by moulding the second polymeric material around the ferromagnetic heating element, so that the ferromagnetic heating element is embedded or partly 15 embedded therein. Other forming methods such as casting or extruding can be used as appropriate. An advantage of the present invention is that the polymeric material of the insert can be chosen to be compatible with the polymeric material of the surface layer of the pipes, 20 whilst the material of the body of the fitting can remain unchanged. This can also enable pipes of dissimilar materials to be joined using a single fitting and an appropriate choice of polymeric material inserts. For example, the fitting can be used to join together cross- 25 linked polyethylene, PVC and modified PVC pipes using the appropriate polymeric material inserts. The ferromagnetic heating element is preferably wholly embedded in the second polymeric material, so that it is





protected from damage when a pipe is inserted into the fitting.

The moulding of the second polymeric material around the  
5 ferromagnetic heating element provides a reservoir of  
fusible material adjacent the heating element in  
preparation for the fusion step. The second polymeric  
material can also be shaped so that the insert is an  
accurate dimensional fit in the body of the fitting, and  
10 the moulded material can be extended axially of the  
ferromagnetic heating element to form in-situ pre-moulded  
"cold zones" to contain the flow of melt from the melt  
region.

15 In a further embodiment, the second polymeric material  
can also have end sections moulded to perform other  
functions. In addition to, or instead of, providing  
"cold zones", the end sections of the moulded second  
polymeric material can, for example, be provided with  
20 internal grooves for accommodating sealing means, for  
example, resilient gaskets or O-rings. Such gaskets or  
O-rings also have the advantage that they can help to  
prevent particles of dust or other contaminants from  
entering the melt region when a pipe is inserted into the  
25 fitting. Preferably, the inner diameter of the insert is  
substantially equal to the outer diameter of the end  
section of the pipe to be connected, with as small a  
clearance as possible consistent with the ability to push

the pipe into the fitting by hand against any frictional resistance. The end section of the pipe can of course have a reduced diameter, allowing the outer diameter of the fitting to be reduced, for example, in no-dig applications. The inner diameter of the insert can also be varied along its length, or two inserts used of different diameter, where pipes of different outer diameter are to be connected. This can, for example, enable the fitting to be used as a reducer.

10

The ferromagnetic heating element preferably has a Curie temperature that is at least 10°C, more preferably from 20°C to 80°C greater than the crystalline melting point or softening point of the second polymeric material.

15

In a preferred method according to the invention, once the body, or the appropriate regions thereof, have been expanded, it is merely necessary to bring the body into the desired location with respect to the insert, and allow the expanded body to recover into contact with the insert. Preferably the dimensions of the body and the insert are such that there is still some unresolved recovery in the body after it has contacted the insert. This unresolved recovery, which, due to the presence of the cross-links, cannot readily be dissipated by the body, enables the body to grip the insert tightly, and, when the insert is softened by heating, the unresolved recovery forces can exert a pressure on the melt region,

thereby improving the quality of the fusion joint. It should be pointed out that this unresolved recovery is not solely due to thermal contraction, or orientation effects, though these may play a part, but to a deformation and strain of the cross-linked polymer structure, which provides a more permanent and reliable recovery force.

Whilst in general it is preferred that the insert produces a fusion bond to the outer surface of the pipe and the inner surface of the body of the fitting, this may not be necessary in all circumstances. Thus, for example, it may not be necessary for the insert to make a full fusion bond to the inner surface of the body of the fitting where the body exerts a significant recovery force on the melt region. In this case, the recovery force may be sufficient to provide the necessary joint tightness, assisted by the end regions of the body, which can be arranged to shrink around the insert, thereby preventing the insert from being extracted from the body of the fitting.

Certain preferred embodiments of the invention will now be described, by way of example only, with reference to the accompanying Drawings in which:

Figure 1 shows a perspective view of a body of an heat fusion coupler, with expansion mandrels positioned prior to the expansion step;

- 5 Figure 2 shows a sectional side elevation of the body of Figure 1 with its end regions expanded by the mandrels;

Figure 3 shows a sectional side elevation of the expanded body of Figure 2 with the inserts positioned for  
10 insertion;

Figure 4 shows a sectional side elevation of the body of Figure 3 with the inserts positioned in the expanded ends; and

15

Figure 5 shows a sectional side elevation of a completed heat fusion coupler according to the invention.

Referring firstly to Figure 1, the body 1 comprises an  
20 extruded tubular member formed by cutting to length an extruded tube of cross-linked polyethylene. The mandrels 2,3 are positioned at the ends of the body 1, and are moved axially towards the body in order to expands the end regions 4,5, leaving an unexpanded central region 6.

25

In Figure 3 the mandrels have been removed. The expanded body is dimensionally unstable and will attempt to revert to its unexpanded state at room temperature.

This process is, however, time dependent, and can take up to several minutes. Whilst the body is still expanded, inserts 7,8 are brought into register on support members 9,10 as shown in Figure 3. Each of the inserts 7,8  
5 comprises a coil of ferromagnetic heating wire 11,12 embedded in a fusible uncross-linked polyethylene matrix 13,14.

Figure 4 shows the inserts (7,8) in position in the  
10 expanded body, still mounted on the support members 9,10. As the body contracts around the inserts, the support members are removed, leaving the inserts firmly held by the body, as shown in Figure 5. Further contraction of  
15 stresses in the body remain unresolved. Thus, when the heat fusion coupler is in use, and the heating elements 11,12 are activated, the body end regions 4,5 continue to exert a recovery force on the fused uncross-linked polyethylene matrices 13,14 and helps to eliminate void  
20 formation and improve the strength of the fusion bond.

It will be appreciated that whilst the support members 9, 10 are indicated as being removed in Figure 5, in a still further embodiment, the members 9, 10 could be spigot  
25 members or pipe members which are to be joined using the heat fusion coupler. In such a case, the members 9, 10 would of course remain in place, whereupon, after contraction of the body, the heating elements 11, 12 are

activated in order to make a fusion between the polyethylene matrices 13, 14 and the members 9, 10.

The reader's attention is directed to all papers and documents which are filed concurrently with or previous to this specification in connection with this application and which are open to public inspection with this specification, and the contents of all such papers and documents are incorporated herein by reference.

10

All of the features disclosed in this specification (including any accompanying claims, abstract and drawings), and/or all of the steps of any method or process so disclosed, may be combined in any combination, except combinations where at least some of such features and/or steps are mutually exclusive.

Each feature disclosed in this specification (including any accompanying claims, abstract and drawings), may be replaced by alternative features serving the same, equivalent or similar purpose, unless expressly stated otherwise. Thus, unless expressly stated otherwise, each feature disclosed is one example only of a generic series of equivalent or similar features.

25

The invention is not restricted to the details of the foregoing embodiments. The invention extends to any novel one, or any novel combination, of the features

disclosed in this specification (including any accompanying claims, abstract and drawings), or to any novel one, or any novel combination, of the steps of any method or process so disclosed.

CLAIMS

- 5 1. A method for the manufacture of a heat fusion fitting, which comprises:
- 10 i) forming a body comprising at least a first layer of a first cross-linked polymeric material,
- 15 ii) embedding or partly embedding a ferromagnetic heating element in a second polymeric material to form an insert, the ferromagnetic heating element having a Curie temperature equal to or greater than the crystalline melting point or softening point of the second polymeric material, and
- 20 iii) assembling the body and the insert to form the fitting.
2. A method according to Claim 1, in which the first layer is an outer layer of the body and the insert
- 25 is positioned internally of the body.



3. A method according to claim 1 or 2, in which the body is shaped such that it can be produced by a continuous extrusion method.
- 5 4. A method according to any of Claims 1 to 3, in which the body is of hollow, tubular construction.
5. A method according to any of the preceding claims, in which the body is of dual layer or multi-layer construction, and at least one of the layers is a  
10 barrier layer.
6. A method according to any of the preceding claims, in which the body is of tubular construction with  
15 either corrugations or ribs on its outer surface.
7. A method according to any of the preceding claims, in which the first polymeric material is polyethylene, an ethylene co-polymer, PVC, or a  
20 modified PVC.
8. A method according to any of the preceding claims, in which the first polymeric material has been cross-linked by a chemical cross-linking method.  
25
9. A method according to any of the preceding claims, in which the first polymeric material is cross-linked to an extent of from 30% to 95%.

10. A method according to any of the preceding claims,  
in which the body and the insert are assembled by  
imparting a degree of dimensional recoverability to  
the body, such that the body, or a portion thereof,  
5 can recover from a larger diameter to a smaller  
diameter and thereby engage the insert which is  
positioned in the direction of recovery.
11. A method according to claim 10, in which the fitting  
10 is an in-line coupling and only the end sections of  
the coupling are expanded.
12. A method according to claim 10 or 11, in which the  
expansion of the body is in the range of from 15% to  
15 45%.
13. A method according to any of the preceding claims,  
in which the ferromagnetic heating element comprises  
20 a wire of conductive material covered with a  
ferromagnetic material.
14. A method according to any of the preceding claims,  
in which the ferromagnetic heating element is of  
25 generally tubular construction and is inwardly  
radially deformable.

15. A method according to any of the preceding claims,  
in which the second polymeric material is uncross-  
linked polyethylene.
- 5 16. A method according to any of the preceding claims in  
which the insert is formed by moulding the second  
polymeric material around the ferromagnetic heating  
element so that the ferromagnetic heating element is  
embedded or partly embedded therein.
- 10 17. A method according to claim 16, in which the moulded  
material is extended axially of the ferromagnetic  
heating element to form end sections adapted to  
perform further functions.
- 15 18. A method according to claim 17, in which the moulded  
material is extended axially of the ferromagnetic  
heating element to form in-situ pre-moulded "cold  
zones" to contain the flow of melt from the melt  
20 region.
19. A method according to claim 17, in which the end  
sections are provided with internal grooves for  
accommodating sealing means.
- 25 20. A method according to any of the preceding claims,  
in which the ferromagnetic heating element has a  
Curie temperature of from 20°C to 80°C greater than

the crystalline melting point or softening point of the second polymeric material.

21. A method according to any of the preceding claims,  
5 in which the dimensions of the expanded body and the insert are such that there is still some unresolved recovery in the body after it has recovered into contact with the insert.

10 22. A method according to any of the preceding claims, substantially as hereinbefore described.

23. A heat fusion fitting comprising a body comprising  
at least a first layer of a first cross-linked  
15 polymeric material, a second layer of a second polymeric material, and a ferromagnetic heating element, the ferromagnetic heating element being embedded or partly embedded in the second layer and having a Curie temperature equal to or greater than  
20 the crystalline melting point or softening point of the second polymeric material.

24. A fitting according to claim 23, in which the first  
layer is an outer layer of the body, the second  
25 layer is an inner layer of the body and the insert is positioned internally of the body.

25. A fitting according to claim 24 or 25, in which the body of the fitting is of hollow tubular construction.
- 5 26. A fitting according to any of claims 23 to 25, in which the body is of dual layer or multi-layer construction, and at least one of the layers is a barrier layer.
- 10 27. A fitting according to any of claims 23 to 26, in which the body is of tubular construction with either corrugations or ribs on its outer surface.
- 15 28. A fitting according to any of claims 23 or 27, in which the body of the fitting has been shaped by a continuous extrusion method.
- 20 29. A fitting according to any of claims 23 to 28, in which the first polymeric material is polyethylene or an ethylene co-polymer.
30. A fitting according to any of claims 23 to 29, in which the first polymeric material has been cross-linked by a chemical cross-linking method.
- 25 31. A fitting according to any of claims 23 to 30, in which the ferromagnetic heating element comprises a

wire of conductive material covered with a ferromagnetic material.

32. A fitting according to any of claims 23 to 31, in  
5 which the second polymeric material is uncross-linked polyethylene.

33. A fitting according to any of claims 23 to 32, in  
10 which the ferromagnetic heating element is wholly embedded in the second polymeric material.

34. A fitting according to any of claims 23 to 33, in  
15 which the ferromagnetic heating element has a Curie temperature of from 20°C to 80°C greater than the crystalline melting point or softening point of the second polymeric material.

35. A fitting according to any of claims 23 to 34, in  
20 which the second layer extends axially of the ferromagnetic heating element to form "cold zones" which, in use, contain the flow of melt from the melt region.

36. A fitting according to any of claims 23 to 34, in  
25 which the second layer has end sections provided with internal grooves for accommodating sealing means.

37. A fitting according to any of claims 23 to 36, in which there is still some unresolved recovery in the body region surrounding the ferromagnetic heating element.

5

38. A fitting according to any of claims 23 to 37, substantially as hereinbefore described with reference to and as illustrated in the accompanying drawings.

10

39. A heat fusion fitting substantially as hereinbefore described.

15

40. A pipe joint formed using a heat fusion fitting according to any of claims 23 to 39.

41. A heat fusion fitting according to any of claims 23 to 39, produced using a method according to any of claims 1 to 22.

20

42. A kit of parts for the manufacture of a heat fusion fitting which comprises:

25

- (i) an insert which comprises a ferromagnetic heating element embedded or partly embedded in a fusible polymeric material, the ferromagnetic heating element having a Curie temperature equal to or greater than the

crystalline melting point or softening point  
of the polymeric material, and

- (ii) a body adapted to receive the insert, the  
5 body comprising at least a first layer of a  
first cross-linked polymeric material.

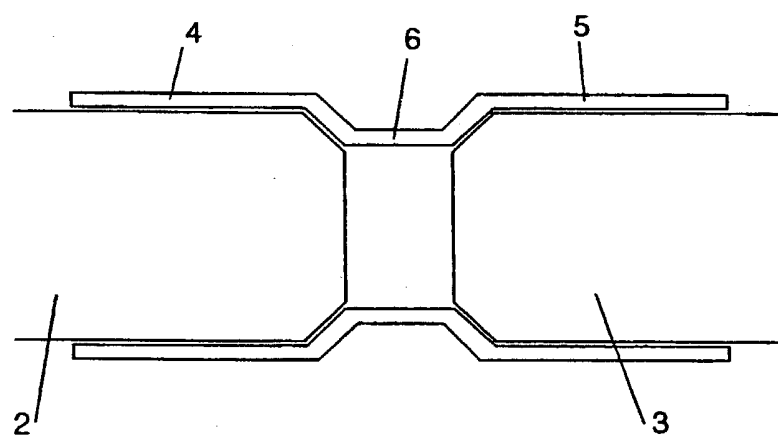
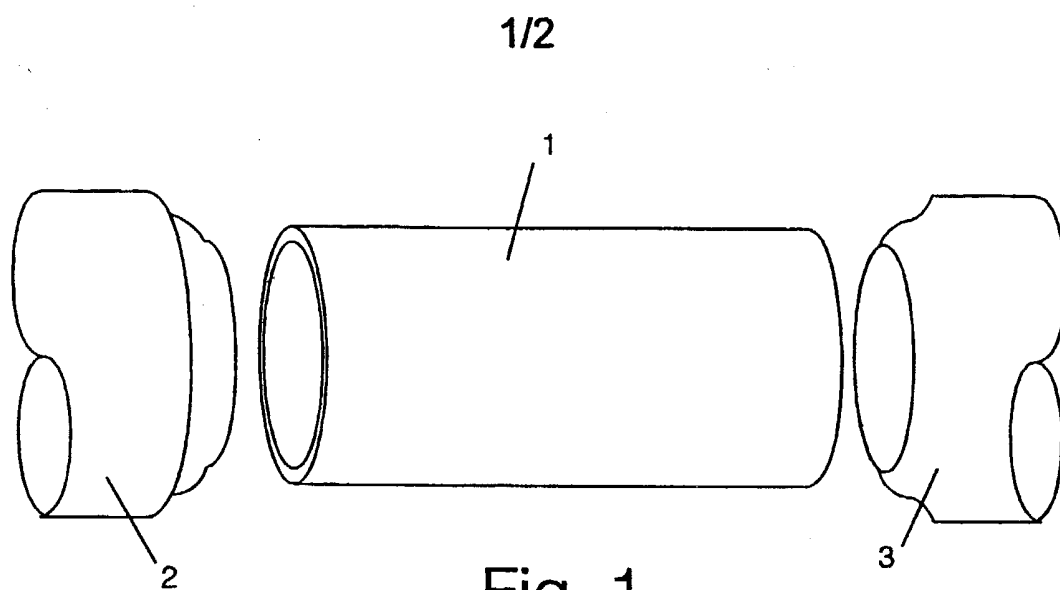
43. A kit of parts for the manufacture of a heat fusion  
fitting which comprises:

10

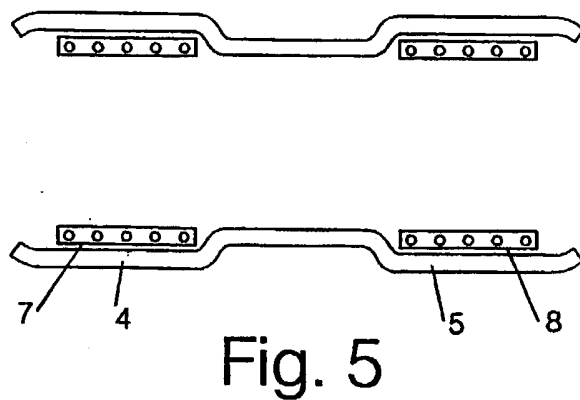
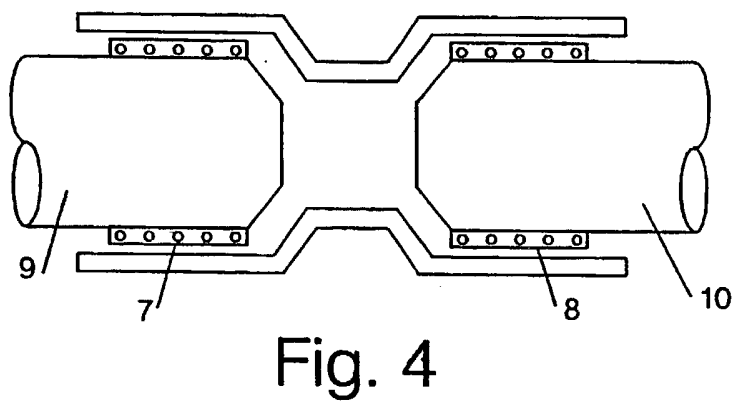
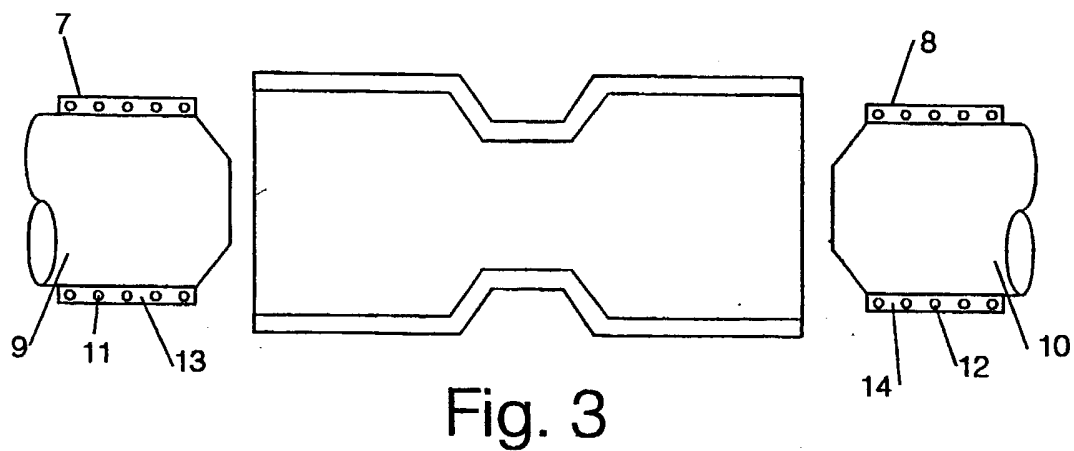
- (i) an insert which comprises a ferromagnetic  
heating element embedded or partly embedded  
in a fusible polymeric material, the  
ferromagnetic heating element having a Curie  
15 temperature equal to or greater than the  
crystalline melting point or softening point  
of the polymeric material, and

- (ii) a body adapted to receive the insert, the  
20 body comprising at least a first layer of a  
first recoverable polymeric material.





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# INTERNATIONAL SEARCH REPORT

Int. J. Application No

PCT/GB 98/01368

## A. CLASSIFICATION OF SUBJECT MATTER

IPC 6 F16L47/00 F16L47/02 B29C61/06 B29C63/18 B29C65/36  
B29C65/68 B29D23/00

According to International Patent Classification(IPC) or to both national classification and IPC

## B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC 6 F16L B29C B29D

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

## C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	EP 0 696 156 A (METCAL INC) 7 February 1996  see page 3, line 10-20 - page 4, line 41-48; figures 2,4	1-5, 14, 16, 20, 23-25, 33, 34, 40-43
A	WO 96 28683 A (RAYCHEM SA NV ;RAYCHEM LTD (GB); BEERSEL JOS VAN (BE)) 19 September 1996 see claim 1; figures 2-4	1-43
A	WO 88 00668 A (BONAZELLI PAOLO) 28 January 1988 see claim 1; figure 1	1-43
-/--		

☒ Further documents are listed in the continuation of box C.

☒ Patent family members are listed in annex.

\* Special categories of cited documents :

"A" document defining the general state of the art which is not considered to be of particular relevance

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"O" document referring to an oral disclosure, use, exhibition or other means

"P" document published prior to the international filing date but later than the priority date claimed

"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention

"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone

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"&" document member of the same patent family

Date of the actual completion of the international search

26 August 1998

Date of mailing of the international search report

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# INTERNATIONAL SEARCH REPORT

In International Application No

PCT/GB 98/01368

## C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT

Category	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	US 4 362 684 A (THALMANN ALFRED) 7 December 1982 cited in the application see claim 1; figures 3-7	1-43
A	WO 87 06182 A (RAYCHEM CORP) 22 October 1987 see claim 1; figures 1,3	1-43
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